

### Stability of interfacial thermal balance in thick β-Ga<sub>2</sub>O<sub>3</sub> crystal **No.:** by edge-defined film-fed growth **P25**

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Abstract

# Results and discussions

1.A furnace structure with larger axial temperature gradient (from 17.40K/mm to 27.46K/mm) over the die was designed by ANSYS FLUENT software.



2.Considering the interface thermal balance and the pressure balance of the meniscus, the relationship between the overheating temperature on the upper surface of the die and the pulling speed was calculated.

# Background

3 Induction Coil

4 Cover 5 Die

6 Crucible 7 Melt

Fig.1 Schematic diagram of EFG method for  $\beta$ - $Ga_2O_3$  ribbon crystals.



The EFG method is commonly used to grow large size  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> 1 Upper Insulation 2 Bottom Insulation single crystals, which have good application prospects in high power electronic devices. When growing n-type thick crystals with high carrier concentration, the growth failure is often caused by the thermal imbalance of the growth interface even with a very slow pulling speed. Thus a larger axial temperature gradient is necessary for n-type  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> crystal growth. The maximum pulling speed is also calculated.



Fig.4 Temperature field in A and B configurations, respectively. The temperature distribution on the upper surface of the die is almost the same. However, in the B configuration, the temperature gradients of the crucible and cover are larger. The axial temperature gradient at the red arrow of the two configurations are 17.40K/mm and 27.46K/mm, respectively. It increases by about 57.5%.



with different carrier concentrations

## Objectives

By changing the thermal field structure and growth process, the appropriate temperature field is designed to solve the problem of thermal imbalance at the crystal growth interface.

The temperature gradient in the crystal is approximated as a reference in calculating the maximum pulling speed.

## Methods



Thermal insulation structure adjustment: Original (A) and adjusted (B)

upper insulation, respectively. The latter has a larger cavity.

Fig.5 The temperature field in B after adding a crystal. Four different positions in the crystal and the function of their die upper surface overheating temperature and pulling speed.

The temperature gradients at four positions a, b, c and d are 7.02K/mm, 7.36 K/mm, 10.92 K/mm and 11.2 K/mm, respectively. The maximum allowable pulling speed at these four positions is calculated, and the crystal center will pull off first, and then the edge. This is consistent with the realistic crystal growth. The speed of 20mm/h is selected for crystal growth experiment. High quality  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> single crystals were obtained through these two improvements.





Growth process adjustment: Considering the pressure balance and heat transfer on the meniscus, the maximum pulling speed at different positions in the crystal is calculated.

Fig.3 A and B upper insulation and meniscus diagram.

$$\gamma \frac{(W_d - W_c)\cos\Psi - 2h\sin\Psi}{h^2} = \rho_l g H + 12\mu v \frac{\rho_s}{\rho_l} \frac{W_c}{W_s^3} H_d$$
$$K_s grad_s = K_l grad_l + \varepsilon \sigma \left( (T_m + \Delta T)^4 - T_m^4 \right) + \rho_s v L_s$$

#### Fig.6 Crystals with unstable (left) and stable (right) growth interface.



The overheated fusing starts from the center of the crystal and then to the edge, which is consistent with the actual growth of the crystal. The pulling speed of 20mm/h was selected for the growth experiment. Through the optimization of thermal field environment and the selection of pulling speed, high-quality two-inch  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> crystals without overheat fusing was realized.